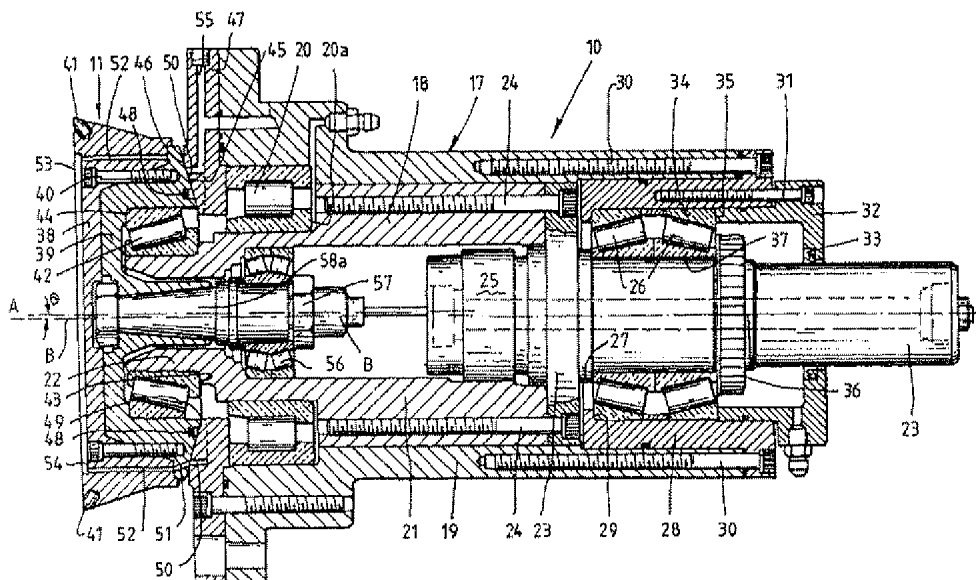




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(54) Title: **ROCK BORING DEVICE**

(57) Abstract

A rock boring device (10) including a rotary disc cutter (11). The disc cutter (11) is driven in an oscillating manner and also driven or free to nutate, and the device includes a mounting section (22) for the rotary disc cutter and a driven section (21), and wherein the mounting section (22) is angularly offset from the axis of the driven section whereby the rotary disc cutter will both oscillate and nutate.

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ROCK BORING DEVICE

Technical Field

The present invention relates to a boring device for creating bore holes in rock, or removing rock from a surface. (For example the floor of a quarry).

Background Art

Boring of holes in rock faces can be conducted in a variety of ways. For example, explosive boring, as the name suggests, involves drilling in the rock face a central primary hole and a series of secondary holes about the primary hole. The secondary holes have a diameter suitable to receive an explosive charge, while the primary holes provides an opening in the rock towards which cracks that are formed in the rock after detonation of the explosive, can propagate. The primary hole is normally of a greater diameter than the secondary holes. Cracks that propagate from the secondary holes to the primary hole create rock chips or segments, that can be separated from the rock being bored and which are thereafter removed, leaving behind a bore hole. The size of the bore hole required determines the number of primary and secondary holes needed, while each explosive detonation can only remove a certain amount of rock, so that the above process may have to be repeated several times to form a bore hole of sufficient cross section and length. As can easily be appreciated this method of boring can be quite dangerous due to the use of explosive material, while it is also time consuming and complicated to prepare the primary and secondary holes in the rock face. Additionally detonation of the explosives is a skilful exercise, as each explosive is detonated separately and at different times, to achieve the greatest extent of crack propagation.

A different form of rock boring involves the use of roller cutters that are rotationally forced into impact with the rock to again create cracks that propagate through

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the rock. The roller cutters employ a plurality of cutting tips, arranged at a variety of different diameters, which are forced into engagement with the rock surface adjacent one another, so that cracks are formed by one cutting tip propagate and intersect with cracks formed by an adjacent tip, thus created a rock chip or segment that can be separated from the rock under the impact of the roller cutter. Applying immense compressive forces to the rock creates the cracks, and eventually a balancing tensile failure occurs. Boring devices of this kind are subject to extensive impact loading because the cutting tips are forced into engagement with the rock under large loads in order to generate the cracks in the rock and thus the rock boring device is required to have facility for large impact absorption. The impact absorption is provided by way of a huge absorption mass attached to the device and the mass is of such a size, that known boring devices can weigh many hundreds of tonnes, a substantial component of which is for impact absorption. As a consequence, the weight and size of these devices makes them expensive to construct and operate.

Disclosure of the Invention

It is an object of the following invention to overcome, or at least reduce one or more of the disadvantages associated with prior art boring devices. It is a further object of the invention to provide a mechanical device of a rotary cutting type, that provides improved rock removal from a rock face to form a rock bore and which is relatively economical to manufacture and operate. The cross section of this bore may be circular, or a polygon, or a planar surface. (Longwall in Coal or a quarry floor).

A rock boring device according to the present invention includes a rotary disc cutter, that in use, is either inserted into a pilot opening formed in the rock

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face, or approaches the rock face at an angle to enable entry.

For this cutting action to be initiated the tip
5 of the disc should initially contact the rock at significant angle. (Probably in excess of 45° , but differing rock types or conditions may reduce or increase this requirement).

10 The boring device is characterised in that the disc cutter is driven in an oscillating manner, and also driven to nutate or free to nutate. The disc cutter is driven to move in this manner about separate or combined oscillating and nutating axes. The nutation angle may be
15 varied or fixed from 0° to almost 90° (Most probably less than 5°). That motion, when applied to the rock face, will cause the disc cutter to apply force to the rock that promotes cracks which propagate toward the rock face adjacent the opening. By this mechanism rock fragments or
20 chips can be separated from the rock when a crack propagates from the wall of the opening to the adjacent rock face. The crack will propagate from a pressure bulb created by the motion of the oscillation, nutation or combination of both motions. This cutting action enables
25 the rock to fail in tension rather than the current traditional compressive first then tension technique. This phenomenon significantly reduces the supporting structure mass for the proposed technology. To insure that the cutting mechanism does not move away from the rock being
30 cut, rather than cut the rock, a mass surrounding the cutter may be necessary.

Brief Description of the Drawings

35 Several preferred embodiments of the invention will now be described with reference to the accompanying drawings, in which:

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Figure 1 is a schematic view of the rock boring device of the preferred embodiment of the present invention and showing the manner in which it makes contact with a rock face,

5

Figure 2 is also a schematic view of the rock boring device showing the manner in which it acts to remove rock material,

10

Figure 3 is a detailed cross-sectional side elevational view of the rock boring device,

Figure 4 is a schematic side elevational view of one example of how the device may be machine mounted to achieve the creation of a bore hole,

15

Figure 5 is a plan view of the machine mounted device of Figure 4, and

20

Figure 6 is a schematic view of another example of how the device may be machine mounted to achieve the creation of a bore hole.

Best Modes for Carrying Out the Invention

25

With reference to Figures 1 and 2 of the drawings, the rock boring device 10 according to this preferred embodiment of the present invention includes a rotary disc cutter 11, that in use, is either inserted into a pilot opening formed in the rock face R, or approaches the rock face at an angle (α) to enable entry (see Figure 1).

30

For this cutting action to be initiated the tip of the disc should initially contact the rock at significant angle. (Probably in excess of 45° , [α] but differing rock types or conditions may reduce or increase this requirement).

35

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The boring device 10 is characterised in that the disc cutter 11 is driven in an oscillating manner, and also driven to nutate or is free to nutate. The disc cutter 11 is driven to move in this manner about separate or combined
5 oscillating and nutating axes. The nutation angle (θ) may be varied or fixed from 0° to almost 90° (Most probably less than 5°). That motion, when applied to the rock face, will cause the disc cutter to apply force to the rock that promotes cracks which propagate toward the rock face
10 adjacent the opening (see Figure 2). By this mechanism rock fragments or chips 12 can be separated from the rock when a crack 13 propagates from the wall of the opening to the adjacent rock face. The crack will propagate from a pressure bulb 14 created by the motion of the oscillation,
15 nutation or combination of both motions. This cutting action enables the rock to fail in tension rather than the current traditional compressive first then tension technique. This phenomenon significantly reduces the supporting structure mass for the proposed technology.

20

Advantageously, the nutating motion of the disc cutter also lends to promote separation of the rock segments from the rock face and may assist sharpening of the contact point of the rotatably mounted disc. Because
25 the disc is rotatably mounted, during each oscillation, the disc will precess. This action provides a new portion of the consumable portion of the disc to the rock and also will assist to distribute the temperature created due to the interaction of the disc and the rock. The cutting
30 action of the tip 15 of the disc will require that the heel 16 of the disc does not contact the rock. To accomplish this a positive 'rake' angle (Ω) must be achieved. This angle may be fixed or varied depending upon the operational mechanism. This angle may also be varied depending upon
35 the rock type of characteristics. The variables being monitored by assessment of the forces within the drive mechanism and surrounding support structure, and the

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results applied to algorithms in an allied computer control system. Depending upon the result of the interpretation of the data, the computer can act to alter angle Ω by providing a suitable signal to a electro-mechanical
5 actuator that can provide the require force to alter the angle of the disc during the cutting action.

A rock boring device according to the invention principally will bore a groove in the rock at circa the
10 diameter of the disc, and at the depth of plunge into the rock. The cutter excavates the rock by generating cracks in the rock and separating rock segments formed by the cracks. However, rock normally will also be removed by the abrasive action of the cutting tips against the rock and
15 the nutating motion of the disc cutter against the rock will also facilitate removal of rock in this manner. However, the amount of rock removed by this mechanism is relatively small. This rock is in the zone referred to previously as the pressure bulb 14.

20

Currently the pressure bulb area or disc to rock contact zone is cooled and airborne dust is controlled by the addition of low pressure water (Less than 10 Bar) applied through the disc via a series of holes. This
25 coolant could also be applied from an external source so that it is directed to contact the tip of the disc area. It may be possible to increase the performance of the system by directing high-pressure water (Probably above 200 Bar) at the pressure bulb area. This jet could be applied
30 either perpendicular to the direction of travel, or in line with the axis of travel, or any angle in between. The water jet indicated as 17 in Figure 2 may enter the crack that is propagating from the pressure bulb and apply a force in equal and all directions, thereby forcing the rock
35 chip to break to the free air side.

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The disc cutter of the boring device preferably has a circular, rock engaging periphery, and may include a plurality of cutting tips which are removably connected to the cutter, but could be permanently connected.

5 Preferably, those tips extend from the disc cutter at or adjacent to the circular periphery thereof either radially, axially, or in a combination of both. The cutting tips can be formed of any suitable material, abrasion resistant, with inherent toughness such as tungsten carbide, alloy and
10 hardened steel, possibly ceramic or other, depending on the type of rock being bored. They can also have any suitable shape and can be fixed to the disc cutter in any suitable manner. The cutter may also be contiguous and be produced of any or a combination of the materials mentioned.

15

The oscillating movement of the disc cutter can be generated in any suitable manner. This motion may be direct mechanical means, or by poly-phase hydraulic pump and motor combination.

20

With reference to Figure 3 of the drawings the cutting device 10 includes a mounting assembly 17 as well as the rotary disc cutter 11. The mounting assembly 17 includes a mounting shaft 18 which is rotatably mounted
25 within a housing 19, that can constitute or be connected to a large mass for impact absorption. The housing 19 thus, can be formed of heavy metal or can be connected to a heavy metallic mass. The shaft 18 is mounted within the housing 19 by a bearing 20, which can be of any suitable type and
30 capacity. The bearing 20 is mounted in any suitable manner known to a person skilled in the art, such as against a stepped section 21.

The housing 19 can have any suitable
35 construction, and in one form includes a plurality of metal plates fixed together longitudinally of the shaft 18. With one such arrangement, the applicant has found that a

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plurality of iron and lead plates provides effective impact absorption based on weight and cost considerations.

The shaft 18 is mounted for rotating motion about
5 a central longitudinal axis AA. The shaft 18 includes a driven section 21 and a mounting section 22. The driven section 21 is connected to drive means 23 at the end thereof remote from the mounting section by any suitable connectors, such as heavy duty threaded fasteners 24, while
10 a seal 25 is applied between the facing surfaces of the mounting section and the drive means.

The drive means 23 can take any suitable form and the means shown in Figure 3 is a shaft that may be driven
15 by a suitable engine or motor. The drive means 23 is mounted within the housing 19 by bearings 26, which are tapered roller bearings, although other types of bearings, either anti friction, plain hydrostatic, or hydrodynamic, that provide radial and axial force reaction could also be
20 employed. With one typical arrangement, the bearings 26 are mounted against a stepped section 27 of the drive means 23 and against a mount insert 28 which is also stepped at 29. The mount insert 28 is fixed by threaded connectors 30 to the housing 19, and fixed to the mount insert 28 by
25 further threaded connectors 31 is a sealing cap 32 which seals against the drive means 23 by seals 33. The sealing cap 32 also locates the outer race 34 of the bearings 26 by engagement therewith at 35, while a threaded ring 36 locates the inner race 37.

30

The mounting section 22 is provided for mounting of the disc cutter 11 and is angularly offset from the axis AA of the driven section 21, which generally will be approximately normal to the rock face being excavated. The
35 axis BB of the mounting section 22 is shown in Figure 3 and it can be seen that the offset angle θ is in the order of a few degrees only. The magnitude of the offset angle θ

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determines the size of the oscillating and nutating movements of the disc cutter 11 and the angle θ can be arranged as appropriate. The angle θ could be zero, but the axis of the eccentric section off-set from the AA axis (Fig 3). This would provide oscillation but no nutation.

The disc cutter 11 includes an outer cutting disc 38 that is mounted on a mounting head 39 by suitable connecting means, such as threaded connectors 40. The outer cutting disc 38 could include a plurality of tungsten carbide cutting bits 41 which are fitted to the cutting disc matrix in any suitable manner. Alternatively, a tungsten carbide ring could be employed. The outer cutting disc can be removed from the cutting device for replacement or reconditioning, by removing the connectors 40.

The disc cutter 11 is rotatably mounted on the mounting section 22 of the mounting shaft 18. The disc cutter 11 is mounted by a tapered roller bearing 42, that is located by a step 43 and a wall 44 of the mounting head 39. An inclined surface 45 of the mounting head 39 is disposed closely adjacent a surface 46 of a mounting insert 47. The surfaces 45 and 46 are spaced apart with minimum clearance to allow relative rotating movement therebetween and the surfaces have a spherical curvature, the centre of which is at the intersection of the axes AA and BB.

A seal 48 is located in a recess 49 of the surface 45 to seal against leakage of lubricating fluid from between the mounting shaft 18, and the housing 19 and the disc cutter 11. A channel 50 is also provided in the surface 45 outwardly of the seal 48 and ducts 51 connect the channel 50 to a further channel 52 and a further duct 53 extends from the channel 52 to a front surface 54 of the outer cutting disc 38. Pressurised fluid can be injected into the various channels and ducts through the port 55 and that fluid is used to flush the underside of the cutting

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disc 38 as well as the relative sliding surfaces 45 and 46.

The disc cutter 11 is rotatably mounted to the mounting section 22 of the mounting shaft 18 by the tapered roller bearing 42 and by a further tapered roller bearing 56. The bearing 56 is far smaller than the bearing 42 for the reason that the large bearing 42 is aligned directly in the load path of the disc cutter and thus is subject to the majority of the cutter load. The smaller bearing 56 is provided to pre-load the bearing 42.

The bearing 56 is mounted against the inner surface of the mounting shaft 18 and the outer surface of a bearing loading facility, comprising a nut 57 and a pre-loading shaft 58. Removal of the outer cutting disc 38 provides access to the nut 57 for adjusting the pre-load of the bearing 56.

The nutating movement of the disc cutter 11, occurs simultaneously with the oscillating motion and that nutating movement is movement in which a point on the cutting edge of the disc cutter is caused to move sinusoidally, in a cyclic or continuous manner as the disc cutter rotates. This movement of the disc cutter applies an impact load to the rock surface under attack, that causes tensile failure of the rock.

The direction of impact of the disc cutter against the rock under face is reacted through the bearing 42 and the direction of the reaction force is substantially along a line extending through the bearing 42 and the smaller bearing 56.

The boring device of the invention is not restricted to a single disc cutter, but can include more than one. For example, the boring device may include three disc cutters arranged along the same plane, but at

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approximately 45° to each other. Such an arrangement can produce a bore of a particular shape, while the speed at which rock is removed is greatly increased. In this arrangement, each of the three disc cutters can be driven
5 by the one drive means, or they may be driven by separate drive means.

Alternatively with reference to Figures 4 and 5 the cutting device 10 may be mounted on a moveable boom 58
10 to enable the disc cutter 11 to be moved about the pilot opening as that opening is enlarged. In this arrangement the housing, and impact absorption mass (if provided) may also be mounted on the boom. The boom may be elevated by an actuator 59 to tilt about a horizontal axis X and
15 pivotable laterally via a turntable 63 about a vertical axis Z by extension and retraction of a pair of rams 64 and 65 extending from cradle 66 to either side of the turntable 63 and mounted on a chassis 70. The boom 58 has shaft 67 therethrough which in turn carries a connector 68 to which
20 the cutting device 11 is pivotably connected at W. The shaft 67 can rotate about its longitudinal axis Y. As a consequence of the pivot axes W, X, Y and Z, the cutting device can be positioned through a whole range of orientations including over one arc dictated by a short
25 radius R_1 about pivot axis W and an arc dictated by a larger radius R_2 about pivot axes X and Z. The entire assembly would be anchored by a clamping means. This may be by vertical anchoring, horizontal anchoring or by
30 application of a mass or adhesive mechanism to ensure the entire vehicle is in a finite position prior to commencing the first cut. Subsequent cuts at the rock face must be referenced to the previous cut to ensure a predetermined depth of cut is maintained. To increase the depth of cut beyond the design limit will cause the surrounding
35 mechanism to engage the rock and stall or cease the cutting action.

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This indexing and the geometry to cut the face can be composed by computer control in order to provide appropriate speed of operation.

5 With reference to Figure 6 of the drawings, in a still further arrangement, a pair of boring devices 10 may be mounted on separate booms 60 and the disc cutters are swept in an arc across the rock face and about pivot points 69, to continually remove successive layers of rock from
10 the face. The entire machine platform 61 must be securely anchored within the bore by gripping mechanisms 62.

 The disc cutters of each device is arranged to sweep in an arc across the rock face being excavated in a
15 first direction D_1 and having completed that sweep, return in the reverse direction D_2 , with each sweep of the disc cutters removing a layer of the rock face. Entrance of the disc cutters into the rock for each successive pass, may be at the cusp C between adjacent concave sections formed by
20 the sweep of each disc cutter.

 The complete machine for the purpose of excavating a tunnel should be mobile and may be mounted on a crawler or on wheels. Providing the carrier or
25 supporting vehicle will fit into the hole size selected, the opening in the rock can be from completely circular at the minimum end of the cutting shape spectrum, to somewhat ovoid. However most customers currently prefer to have a flat floor to enable them to operate subsequent vehicles.

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CLAIMS:

1. A rock boring device including a rotary disc cutter, wherein the disc cutter is driven in an oscillating manner and also driven or free to nutate.
2. A rock boring device as claimed in Claim 1, wherein the device includes a mounting section for the rotary disc cutter and a driven section, and wherein the mounting section is angularly offset from the axis of the driven section whereby the rotary disc cutter will both oscillate and nutate.
3. A rock boring machine, incorporating a rock boring device as claimed in either Claim 1 or 2, wherein the rock boring device is mounted on a boom.
4. A rock boring machine as claimed in Claim 3, wherein the boom is adapted to pivot about a vertical axis.
5. A rock boring machine as claimed in Claim 3 or 4, wherein the boom is adapted to pivot about a horizontal axis.
6. A rock boring machine as claimed in Claim 3 or 4, wherein the rock boring device is supported by said boom whereby as to be pivotable about an axis extending longitudinally of said boom.
7. A rock boring machine as claimed in any one of Claims 3 to 6, wherein the rock boring device is supported to pivot relative to said boom.
8. A rock boring device substantially as hereinbefore described with reference to Figures 1 to 3 of the accompanying drawings.

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9. A rock boring machine incorporating a rock boring device as claimed in Claim 8.

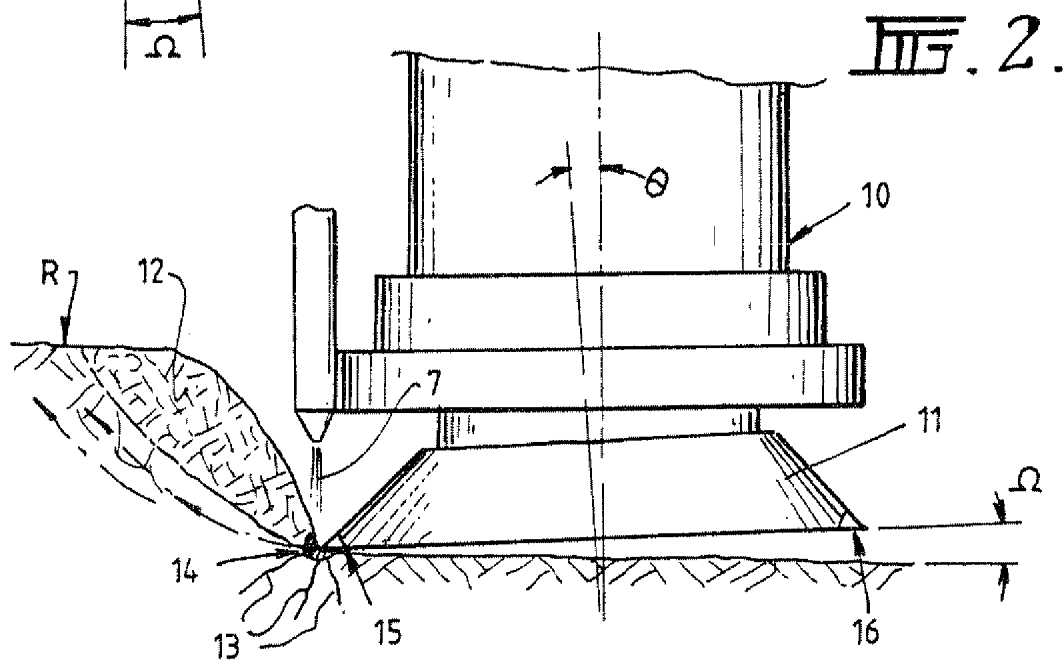
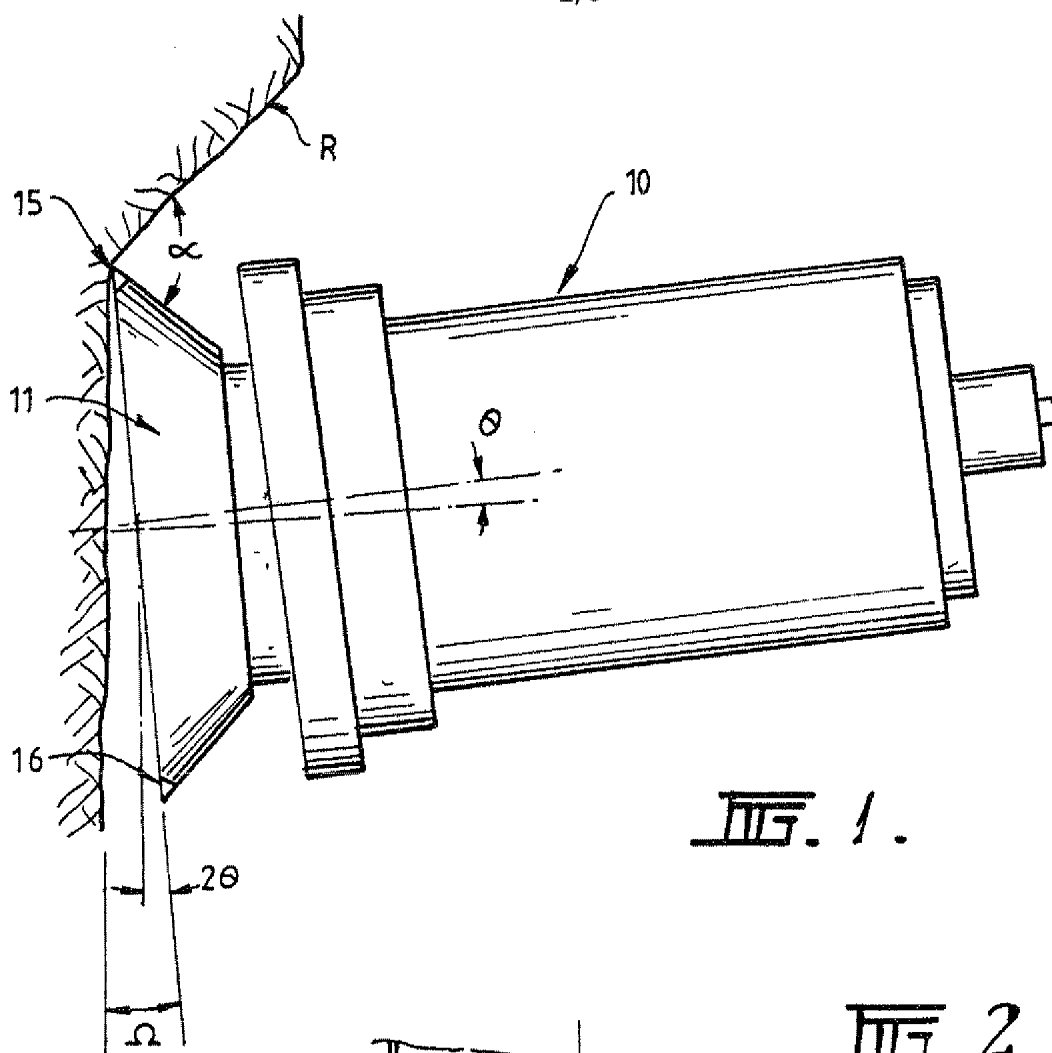
10. A rock boring machine substantially as hereinbefore described with reference to Figures 4 and 5, or Figure 6, of the accompanying drawings.

11. A rock boring machine as claimed in any one of Claims 3 to 7, or Claims 9 and 10, wherein a plurality of said rock devices are carried by the machine.

12. A rock boring machine as claimed in any one of Claims 3 to 7, or Claims 9 to 11, wherein the cutter velocity is controlled by interaction with a computer that processes algorithms with variable information input being provided by strain gauges and accelerometers mounted adjacent to the cutter.

13. A rock boring machine as claimed in any one of Claims 3 to 7, or Claims 9 to 11, wherein the vehicle must be anchored or referenced to a position to insure too greater cut is not applied should the vehicle inadvertently move from the position it was in at the commencement of the cutting cycle.

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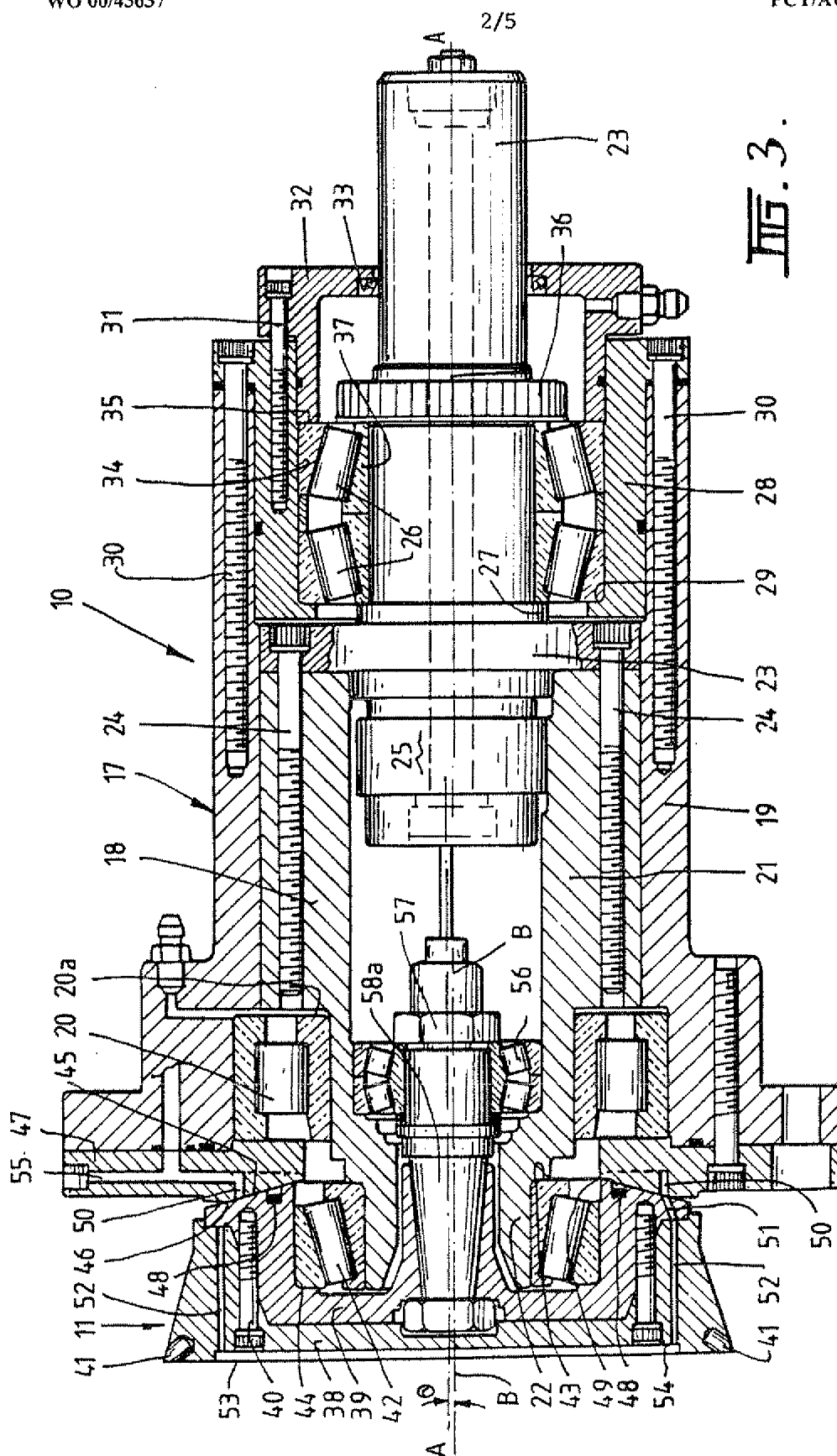


Fig. 4.

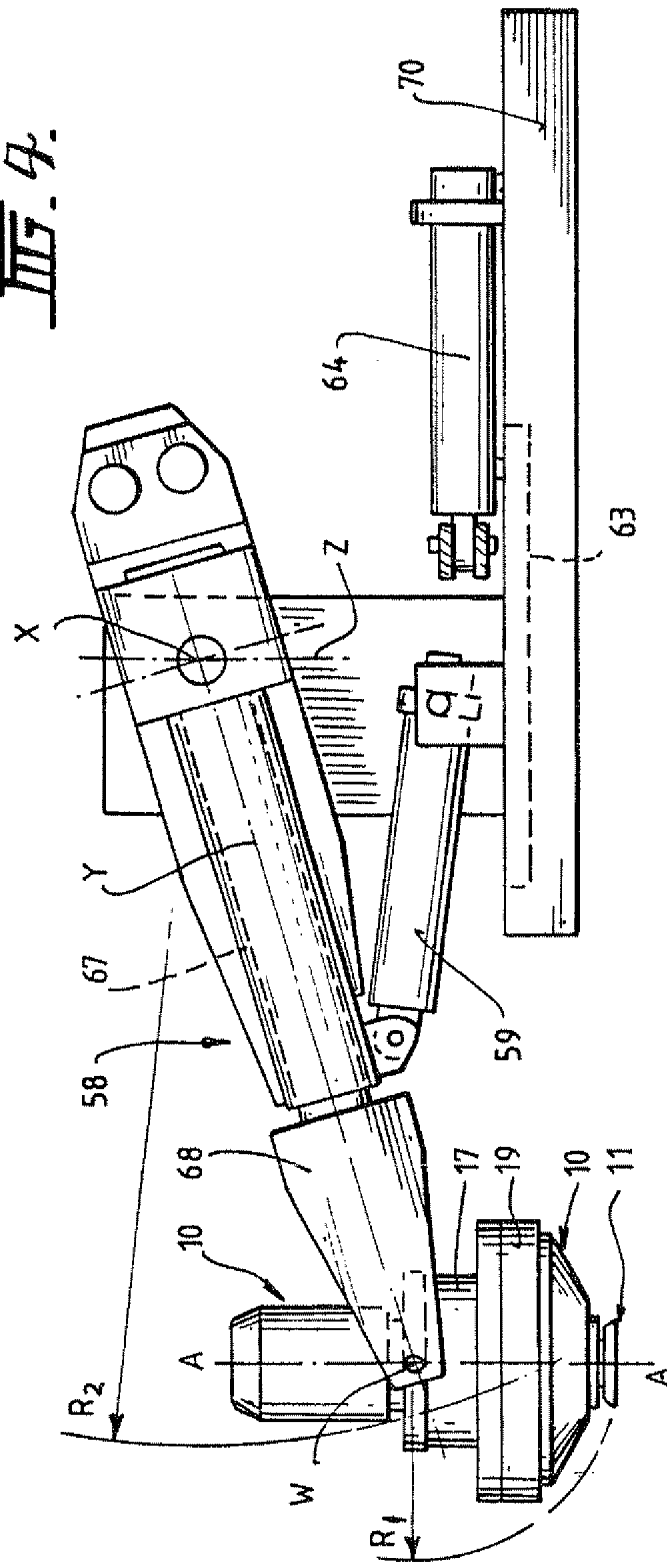
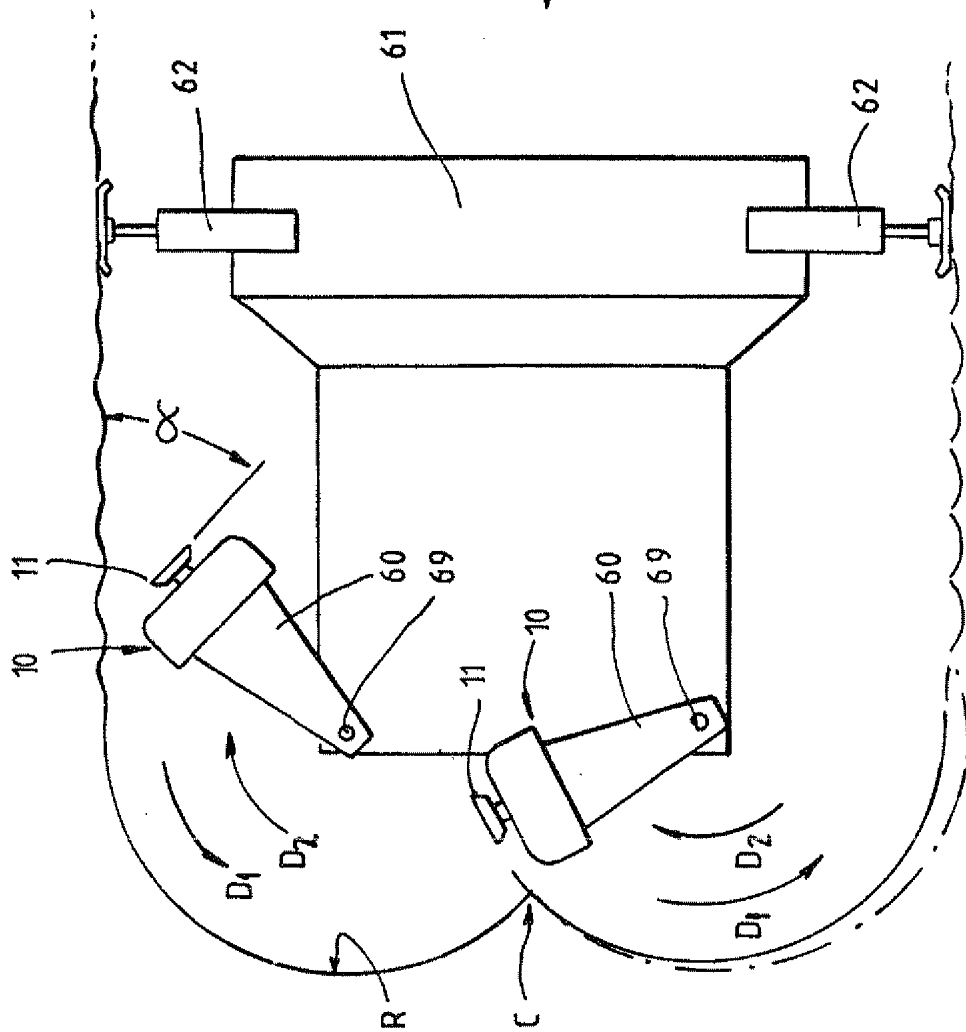


FIG. 6.



INTERNATIONAL SEARCH REPORT

 International application No.
 PCT/AU 00/00030

A. CLASSIFICATION OF SUBJECT MATTER		
Int Cl ⁷ : E21D 9/10		
According to International Patent Classification (IPC) or to both national classification and IPC		
B. FIELDS SEARCHED		
Minimum documentation searched (classification system followed by classification symbols) IPC: E21B 9/10, 9/11 + Keywords		
Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched AU: IPC as above		
Electronic data base consulted during the international search (name of data base and, where practicable, search terms used) WPAT: oscillat+ or wobbb+ or nutat+ or eccent+ or offcent+ or ellipt		
C. DOCUMENTS CONSIDERED TO BE RELEVANT		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	AU 41965/72 B (UNION INDUSTRIELLE BLANZY-QUEST) 20 December 1973 see whole document	1
A	US 5575537 A (PETER KOGLER) 19 November 1996 see whole document	1
A	GB 2252576 A (ANDERSON GROUP PLC) 12 August 1992 see whole document	1
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Name and mailing address of the ISA/AU AUSTRALIAN PATENT OFFICE PO BOX 200 WODEN ACT 2606 AUSTRALIA E-mail address: pct@ipaustalia.gov.au Facsimile No.: (02) 6285 3929	Authorized officer BARRY STEPHENS Telephone No.: (02) 6283 2106	

INTERNATIONAL SEARCH REPORT

International application No.

PCT/AU 00/00030

C (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	EP 692612 A (BECHEM) 17 January 1996 see whole document	1

Information on patent family members

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This Annex lists the known "A" publication level patent family members relating to the patent documents cited in the above-mentioned international search report. The Australian Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

Patent Document Cited in Search Report			Patent Family Member				
AU	41965/72	NONE					
US	5575537	DE	4413235	EP	677643	ZA	9502982
GB	2252576	AU	11788/92	US	5338104	WO	92/14035
		ZA	9200802				
EP	692612	CH	689546				